

ASX/Media Release
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SIGNIFICANT TIN INTERCEPTS FROM GILLIAN DRILLING PROGRAM

Australian tin exploration company, Consolidated Tin Mines (ASX: CSD) is pleased to announce results from its most recent drilling program at the company's Gillian Project in northern Queensland.

The results come from a drilling program carried out during November 2009, which produced significant intercepts of tin mineralisation. The latest program was designed as infill drilling to improve confidence in the extent of mineralisation found in the earlier programs.

Summary highlights include:

Hole 93	20-30 metres downhole	10 metres @ 0.88%Sn, 49.6%Fe
Hole 94	14-47 metres downhole	33 metres @ 0.80%Sn, 40.3%Fe
Hole 95	34-70 metres downhole	36 metres @ 1.20% Sn, 43.5%Fe
Hole 96	53-66 metres downhole	13 metres @ 0.90%Sn, 31.7%Fe
Hole 97	51-58 metres downhole	7 metres @ 0.49%Sn, 38.1%Fe

(See Table 1 for full results).

The Gillian Project is part of Consolidated Tin's wider Mt Garnet Project area, which is located 200km south west of Cairns in the lower Herberton Tin Field, one of Australia's premier tin fields. In addition to tin the company is also assaying for iron.

The Company has now drilled a total of 6,300 metres across 137 holes at the Mt Garnet Project and the project currently has a **total JORC Resource of 5.3Mt @ 0.6% Tin**, which includes a **Measured Resource of 724,700t @ 0.81 Tin** at the Gillian project area.

Managing Director Ralph De Lacey said: "The Company is very pleased with the continuing excellent results from the Gillian project with drilling showing excellence widths and good grades of both tin and iron. Hole 95 with 36metres averaging 1.2% Sn is the best intercept seen to date at the Project."

Assays were undertaken by fused bead XRF by the Burnie Research Laboratory in Tasmania, and results are total tin (Sn) and total iron (Fe).

ENDS

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The information contained in this report that relates to assay results of rock samples and drill chips, to mineral resource estimates and to ore reserve estimates of mineralisation is based on information compiled by John Sainsbury (BSc, AusIMM) an executive director of Consolidated Tin Mines Limited. John Sainsbury is a geologist of 30 years experience and has sufficient experience in the type of mineralisation under consideration to qualify as a Competent Person as defined by the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves - JORC Code, 2004 Edition. John Sainsbury has consented to the inclusion of this information in the form and context in which it appears.

ABOUT CONSOLIDATED TIN MINES LIMITED

Consolidated Tin Mines Limited (CSD) is a junior exploration company with current focus on Tin at Mt Garnet in the lower Herberton tin field in North Queensland.

Short to medium term goals are:

- Further expand resources at Gillian and Deadmans Gully while defining resources of known mineralisation at Pinnacles
- Develop a hard rock mining operation
- Develop an alluvial mining operation
- Explore other known mineralisation within current tenement holding to provide resource expansion

Table 1: Breakdown of Tin JORC Resource

TIN (Sn)	Measured tonnes	Grade %	Indicated tonnes	Grade %	Inferred tonnes	Grade %	Total tonnes	Grade %
Gillian	724,700	0.81	846,100	0.84	1,458,800	0.75	3,029,600	0.79
Pinnacles - Wafer	-	-	218,200	0.49	1,133,100	0.39	1,351,300	0.41
Pinnacles - Sniska	-	-	-	-	306,900	0.32	306,900	0.32
Pinnacles - Hartog	-	-	-	-	212,700	0.51	212,700	0.51
Deadmans Gully	-	-	401,500	0.49	-	-	401,500	0.49
TOTAL	724,700	0.8139	1,465,800	0.69	3,111,500	0.56	5,302,000	0.61

Mt Garnet Key Projects

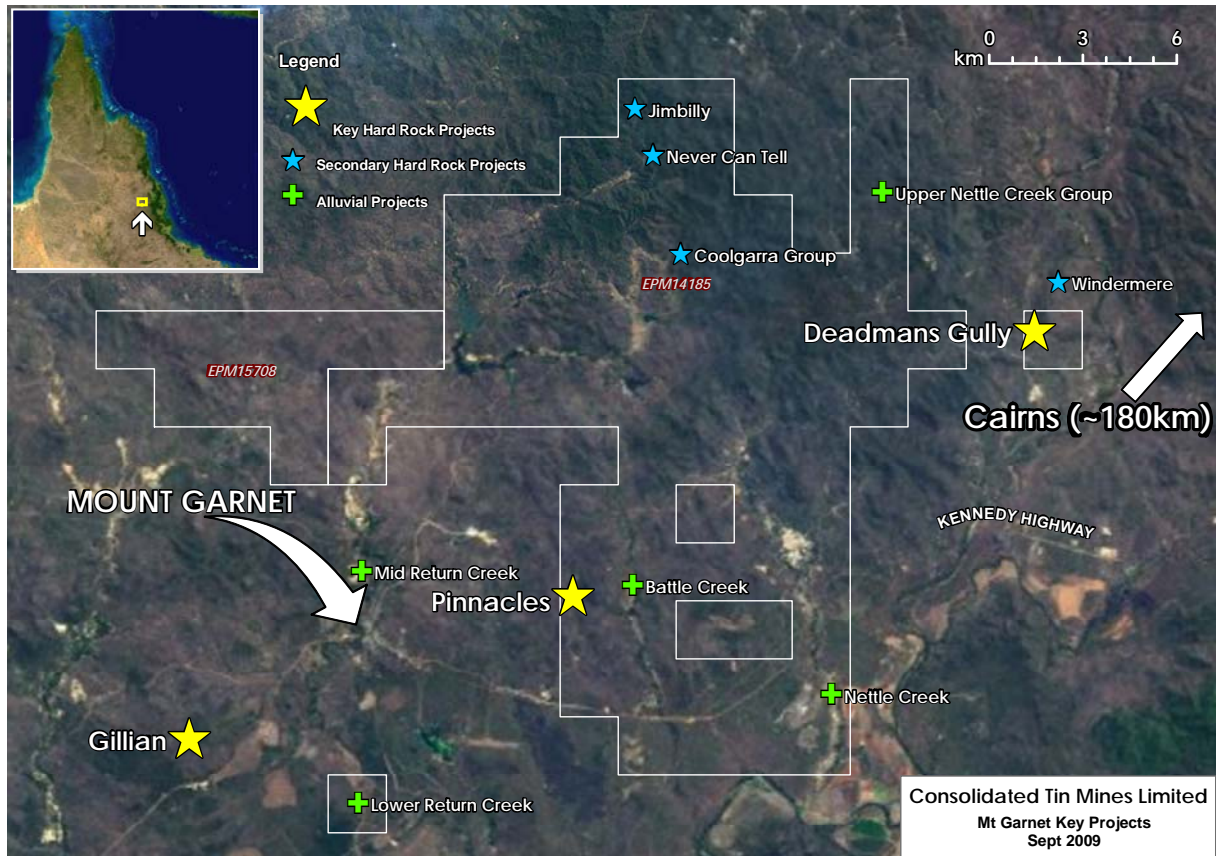
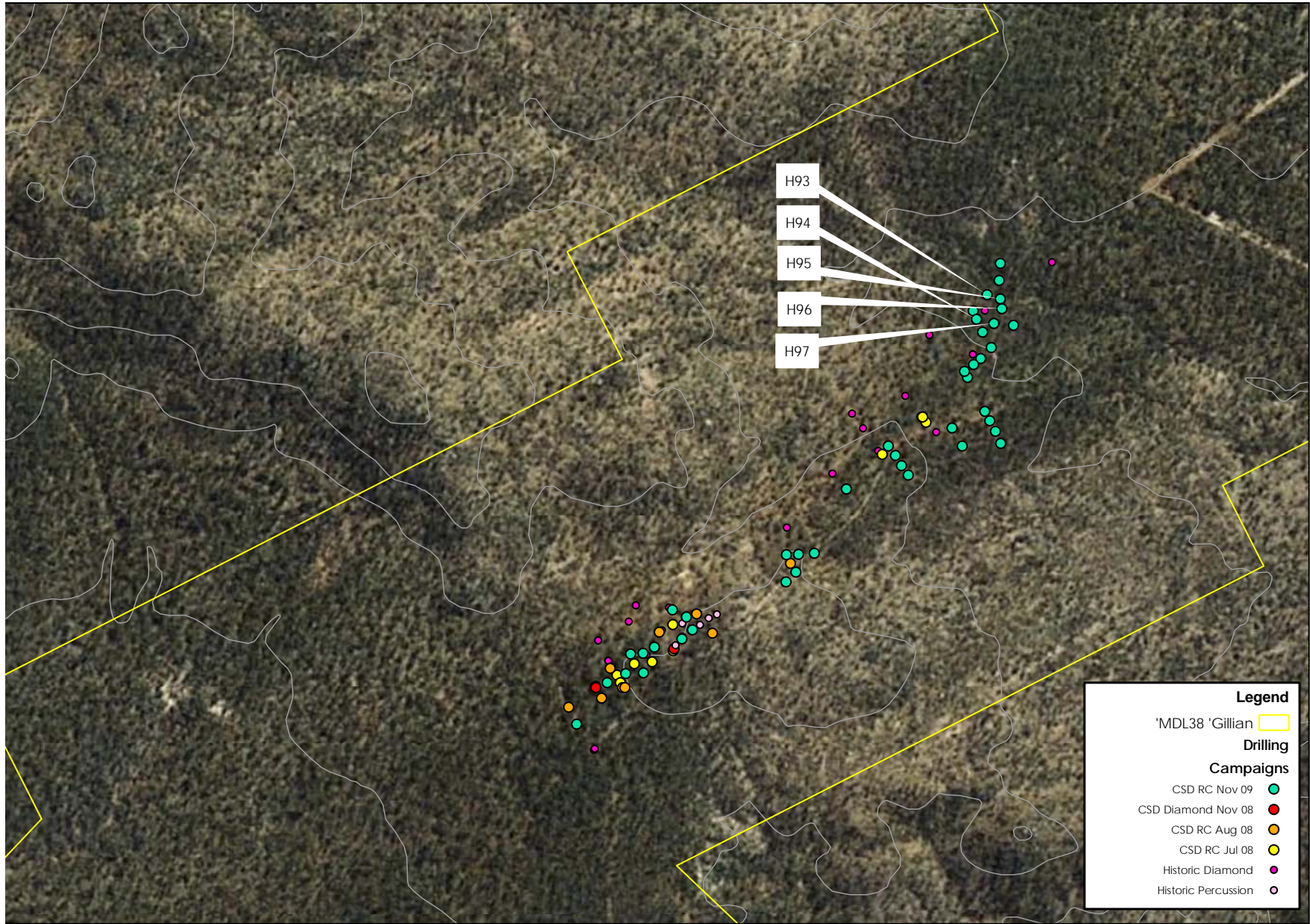


Table 1 – Gillian Drill Locations and Assay Results

Details of drill holes				
Hole No	MGA55 Location	Drill Azimuth (from Mag. North)	Drill Dip	Depth
H93	8041396, 294389	320	-60	54m
H94	8041355, 294371	325	-60	54m
H95	8041388, 294410	320	-60	78m
H96	8041372, 294413	320	-60	72m
H97	8041348, 294400	325	-60	66m

Drill Location Map



Hole	Intercept (m)	%Sn	%Fe
H93 (Gillian)			
	16-17	0.12	11.1
	17-18	0.19	12.3
	18-19	0.13	10.4
	19-20	0.13	26.7
	20 - 21	1.17	48.9
	21 - 22	0.46	59.7
	22 - 23	0.75	56.4
	23 - 24	0.82	53.8
	24 - 25	0.79	53.0
	25 - 26	0.69	59.6
	26 - 27	0.63	58.0
	27 - 28	1.48	44.6
	28 - 29	1.65	45.8
	29 - 30	0.35	15.8
	30 - 31	0.09	12.9
	31 - 32	0.01	5.2
	32 - 33	0.01	4.7
	33 - 34	0.01	4.2
	34 - 35	<0.01	4.1
	35 - 36	0.01	3.4
	36 - 37	0.03	4.7
	37 - 38	0.01	4.1
	38 - 39	0.01	4.1
	39 - 40	0.03	4.2
	40 - 41	0.02	3.6
	41 - 42	0.01	2.7
	42 - 43	0.01	3.7
	43 - 44	0.02	3.7
	44 - 45	0.02	4.5
	45 - 46	0.02	4.0
	46 - 47	0.01	4.4
	47 - 48	0.03	4.2

Hole	Intercept (m)	%Sn	%Fe
H94 (Gillian)			
	14-15	1.99	33.5
	15-16	0.77	26.6
	16-17	1.07	28.4
	17-18	0.43	33.2
	18-19	0.57	29.5
	19-20	0.38	20.5
	20 - 21	0.4	26.7
	21 - 22	0.24	27.8
	22 - 23	0.29	26.1
	23 - 24	0.29	32.0
	24 - 25	0.29	31.7
	25 - 26	0.49	45.0
	26 - 27	1.09	50.6
	27 - 28	1.16	57.8
	28 - 29	1.05	57.2
	29 - 30	0.91	55.0
	30 - 31	1.17	49.6
	31 - 32	0.9	59.4
	32 - 33	0.82	53.2
	33 - 34	0.56	57.6
	34 - 35	0.69	54.4
	35 - 36	0.5	58.7
	36 - 37	0.81	53.0
	37 - 38	0.99	54.8
	38 - 39	1.01	48.9
	39 - 40	1.15	28.9
	40 - 41	1.3	27.1
	41 - 42	1.19	29.6
	42 - 43	1.03	37.6
	43 - 44	0.88	49.8
	44 - 45	0.68	31.1
	45 - 46	1.02	33.5
	46 - 47	0.42	22.6
	47 - 48	0.11	6.9
	48 - 49	0.08	5.1

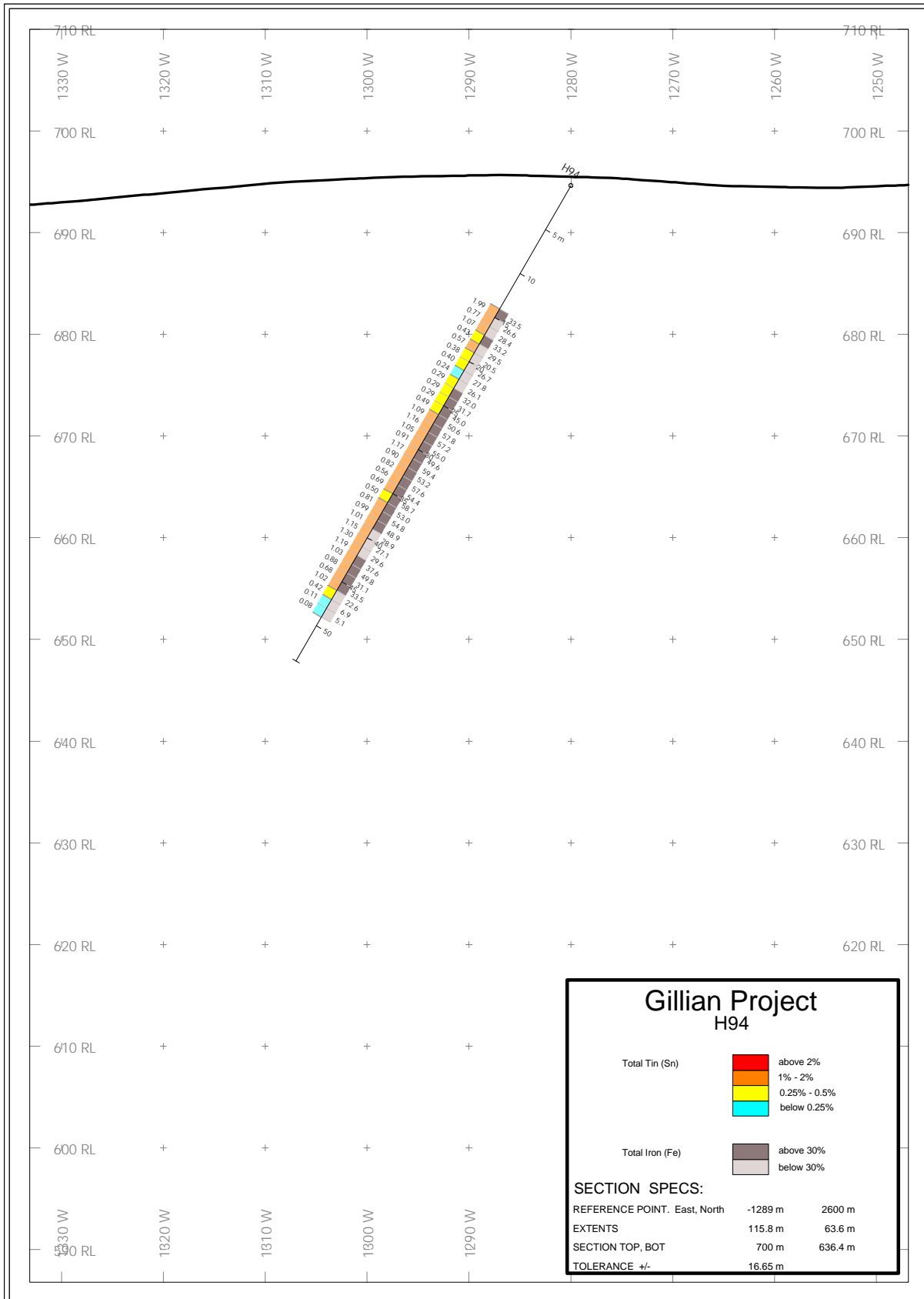
Hole	Intercept (m)	%Sn	%Fe
H95 (Gillian)			
	32 - 33	0.01	6.5
	33 - 34	0.06	9.6
	34 - 35	1.23	34.6
	35 - 36	0.83	28.2
	36 - 37	1.19	45.7
	37 - 38	1.37	55.5
	38 - 39	1.44	36.2
	39 - 40	1.3	38.3
	40 - 41	1.39	59.7
	41 - 42	1.09	60.7
	42 - 43	0.67	56.1
	43 - 44	0.78	43.9
	44 - 45	0.39	29.3
	45 - 46	0.95	31.7
	46 - 47	1.24	38.2
	47 - 48	1.48	51.6
	48 - 49	1.72	47.1
	49-50	1.28	48.6
	50-51	0.64	31.4
	51-52	0.51	51.2
	52-53	0.61	54.0
	53-54	0.62	41.5
	54-55	0.77	39.5
	55-56	0.74	37.7
	56-57	0.74	44.2
	57-58	1.04	46.2
	58-59	1.62	48.0
	59-60	1.73	45.6
	60-61	1.67	44.1
	61-62	1.85	49.4
	62-63	1.85	50.5
	63-64	1.68	51.5
	64-65	2.68	47.4
	65-66	2.89	47.1
	66-67	0.36	20.1

Hole	Intercept (m)	%Sn	%Fe
H95 (Gillian)			
	67-68	1.1	35.1
	68-69	1.07	46.9
	69-70	0.57	29.8
	70-71	0.08	15.0
	71-72	0.25	23.5
	72-73	0.04	6.2
	73-74	0.03	5.1
	74-75	0.04	6.0
	75-76	0.03	5.8
	76-77	0.05	7.2
	77-78	0.09	5.7

Hole	Intercept (m)	%Sn	%Fe
H96 (Gillian)			
	40 - 41	0.22	13.0
	41 - 42	0.26	14.3
	42 - 43	0.2	26.5
	43 - 44	0.09	18.0
	44 - 45	0.16	16.8
	45 - 46	0.07	18.1
	46 - 47	0.1	13.0
	47 - 48	0.11	14.6
	48 - 49	0.31	13.8
	49-50	0.09	7.4
	50-51	0.02	21.3
	51-52	0.01	12.9
	52-53	0.01	5.1
	53-54	1.25	51.6
	54-55	0.69	58.5
	55-56	1.36	32.1
	56-57	1.07	40.3
	57-58	1.96	43.8
	58-59	1.63	30.5
	59-60	0.24	8.3
	60-61	0.95	20.6
	61-62	0.83	48.6
	62-63	0.77	34.6
	63-64	0.49	20.1
	64-65	0.24	11.9
	65-66	0.23	11.6
	66-67	0.05	6.2
	67-68	0.04	3.1
	68-69	0.05	3.9
	69-70	0.04	4.1
	70-71	0.02	1.3
	71-72	0.01	1.2

Hole	Intercept (m)	%Sn	%Fe
H97 (Gillian)			
	40 - 41	0.06	7.9
	41 - 42	0.12	9.0
	42 - 43	0.06	5.8
	43 - 44	0.05	7.4
	44 - 45	0.02	14.4
	45 - 46	0.01	15.4
	46 - 47	0.02	11.0
	47 - 48	0.02	8.6
	48 - 49	0.01	17.2
	49-50	0.02	21.8
	50-51	0.04	25.5
	51-52	0.3	35.0
	52-53	0.33	34.9
	53-54	0.81	37.3
	54-55	0.53	48.7
	55-56	0.54	51.5
	56-57	0.5	35.7
	57-58	0.43	23.5
	58-59	0.07	11.1
	59-60	0.09	5.5
	60-61	0.04	2.6
	61-62	0.02	1.5
	62-63	0.02	1.4

Hole 94
Section 2590N



Hole 95 & 96
Section 2640N

