

# CONSOLIDATED

## TIN MINES LIMITED

ASX/Media Release  
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### MAJOR JORC RESOURCE UPGRADE AT GILLIAN TIN PROJECT

#### Key points

- Measured Resource increased to 1.2Mt @ 0.93% Tin; represents a 478,300t increase on the previous Measured Resource
- The new Indicated Resource is 824,100t @ 1.0% Tin; represents a significant increase in Tin grade of 20%
- Latest drilling results confirm potential to develop the project into a near-surface, low cost tin mining operation
  - 25 intersection over 10 metres in length at better than 0.5%Sn
  - Hole 95; 36 metres @ 1.2%Sn, 43.5% Fe
  - Hole 129; 24 metres @ 1.45%Sn, 36.1% Fe (includes 11m of 2.15% Sn and 1m of 6.3%Sn)
- Gillian mineralisation is open along strike in all directions and at depth, and is outcropping in places
- The Gillian Project is part of the wider Mt Garnet Tin project area The Company has drilled a total of 6,300m across 137 holes at the Mt Garnet Project to date
- In addition to Tin the company is also assaying for iron

Consolidated Tin Mines Ltd (ASX: CSD) is pleased to announce a major JORC Resource upgrade at the Company's Gillian Tin Project in northern Queensland.

The JORC Measured Resource at the Gillian Project has increased to 1.2 million tonnes @ 0.93% Tin (Sn) from the previous Measured Resource of 724,700 tonnes @ 0.8% Tin. The new JORC Indicated Resource is 824,100 tonnes @ 1.0% Tin (Sn). This represents a significant increase in the Tin grade of 20%.

A breakdown of the Resource Upgrade is shown in Table 1 below;

Table 1: Upgraded JORC Resource at Gillian Tin Project

TIN (Sn)	Measured tonnes	Grade %	Indicated tonnes	Grade %	Inferred tonnes	Grade %	Total tonnes	Grade %
Gillian	1,203,000	0.93	824,100	1.00	974,100	0.83	3,001,300	0.91
Pinnacles - Wafer	-	-	218,200	0.49	1,133,100	0.39	1,351,300	0.41
Pinnacles - Sniska	-	-	-	-	306,900	0.32	306,900	0.32
Pinnacles - Hartog	-	-	-	-	212,700	0.51	212,700	0.51
Deadmans Gully	-	-	401,500	0.49	-	-	401,500	0.49
<b>TOTAL</b>	<b>1,203,000</b>	<b>0.93</b>	<b>1,443,800</b>	<b>0.78</b>	<b>2,626,800</b>	<b>0.55</b>	<b>5,273,700</b>	<b>0.70</b>

Cut-off grade used was 0.2% Sn

The Resource upgrade has been determined based on results from Consolidated Tin's latest drilling program at the Gillian Project, which was conducted in November-December 2009.

The last group of assay results from this drill program have continued to produce further significant intercepts of tin mineralisation, and summary highlights of these drill assay results include:

**Table 2**

<i>Hole No</i>	<i>Downhole Intercept</i>	<i>Length and Grade</i>
Hole 128	7-13 metres 16-27 metres	6 metres @ 1.01% Sn, 26.5%Fe 11 metres @ 0.74% Sn, 26.9% Fe
Hole 129	9-33 metres	24 metres @ 1.45% Sn, 36.1% Fe
<i>[Hole 129 contains a one metre interval of 6.29% Sn from 15-16 metres downhole, and from 15-26 metres downhole it contains an 11 metre interval @ averages 2.15% Sn]</i>		
Hole 130	83-90 metres	7 metres @ 1.23% Sn, 34.2% Fe
Hole 133	10-12 metres 37-41 metres	2 metres @ 0.77% Sn, 19.1% Fe 4 metres @ 0.88% Sn, 18.4% Fe
Hole 134	55-60 metres 108-114 metres	5 metres @ 0.31% Sn, 14.8% Fe 6 metres @ 0.39% Sn, 13.8% Fe
Hole 135	11-15 metres 29-44 metres	4 metres @ 0.87% Sn, 27.0% Fe 15 metres @ 1.02% Sn, 39.6% Fe
Hole 136	48-68 metres	20 metres @ 0.84% Sn, 29.9% Fe

The Gillian Project is part of Consolidated Tin's wider Mt Garnet Project area, which is located 200km south west of Cairns in the lower Herberton Tin Field, one of Australia's premier tin fields (See Figure 4, attached, for Projects Location Map). The Company has drilled a total of 6,300 metres across 137 holes at the Mt Garnet Project and the project currently has a **total JORC Resource of 5.2Mt @ 0.70% Sn, 5.2Mt @ 26.45 Fe & 0.96Mt @ 15.25% F**.

The mineralisation is open ended with magnet/geophysics interpretations indicating extensions of strike at both ends. There is also potential for extensions at depth.

Figure 1: Hole location for above summary

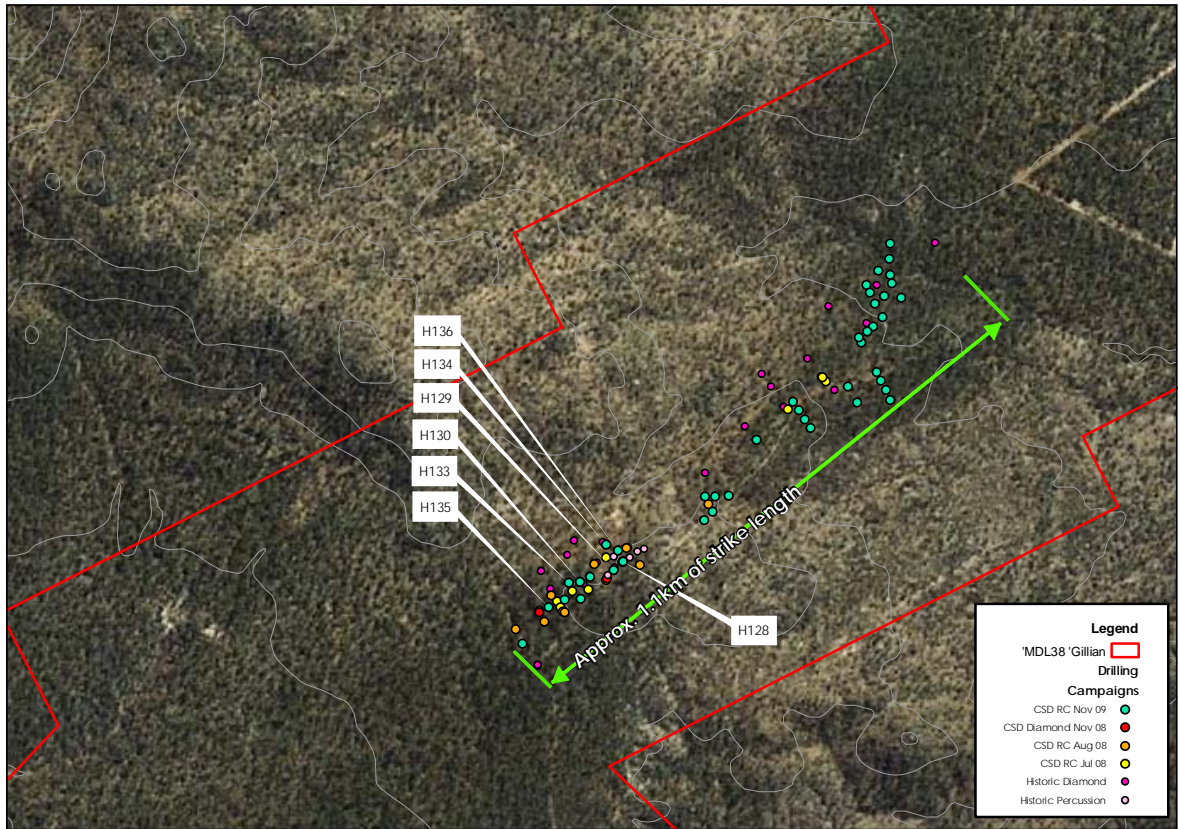


Figure 2 : Mt Garnet area showing Key Project locations

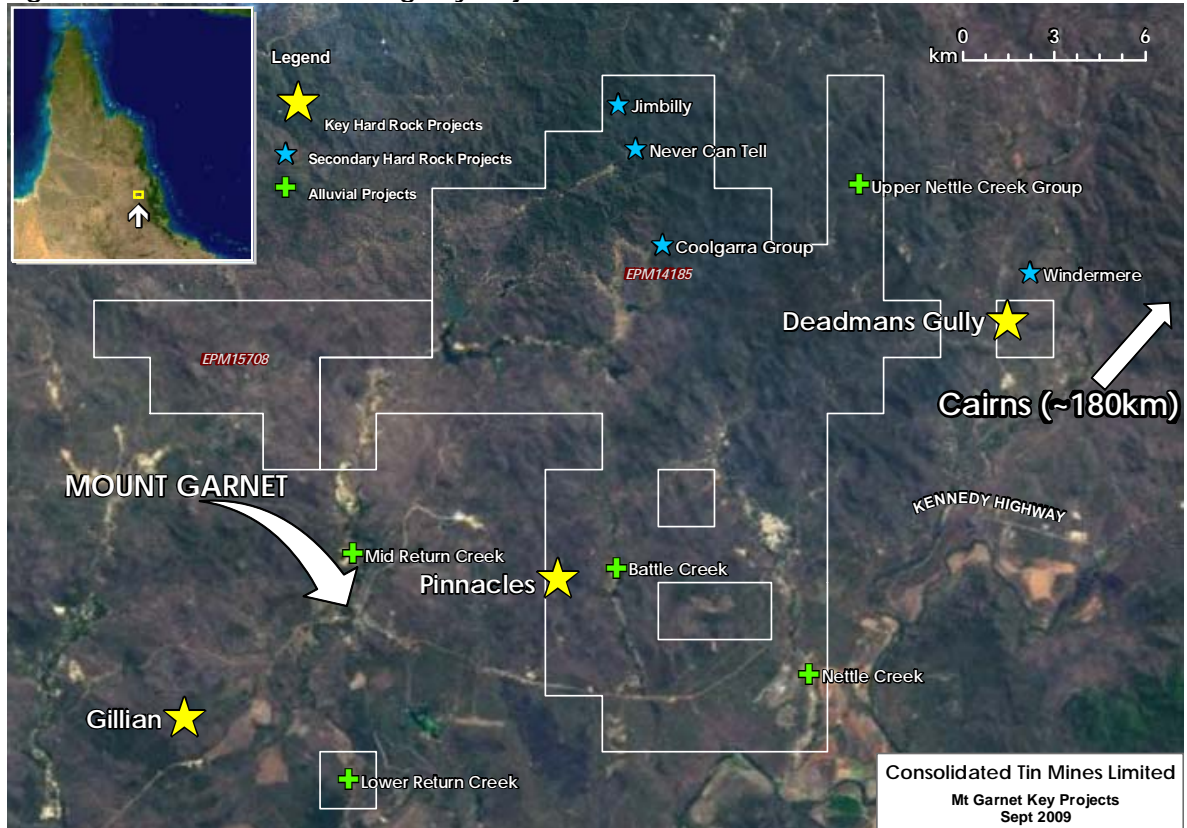


Figure 3 : Gillian Deposit Outcropping





Drilling to date at the Gillian Project has produced 25 very significant tin intersections that exceed 10 metres in length with grades of better than 0.5% Sn. Details of these are shown in **Table 3**, attached;

Consolidated Tin Managing Director Ralph De Lacey said: "We are delighted with the continuing success of our drilling programs at the Gillian Project, which has culminated in our latest JORC Resource upgrade at the project. The significant upgrade in Measured and Indicated Resource categories confirms our confidence in the development potential of the project into a major, low cost, open cut tin mining operation."

Assays were undertaken by fused bead XRF by the Burnie Research Laboratory in Tasmania, and results are total tin (Sn) and total iron (Fe).

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The information contained in this report that relates to assay results of rock samples and drill chips, to mineral resource estimates and to ore reserve estimates of mineralisation is based on information compiled by John Sainsbury (BSc, AusIMM) an executive director of Consolidated Tin Mines Limited. John Sainsbury is a geologist of 30 years experience and has sufficient experience in the type of mineralisation under consideration to qualify as a Competent Person as defined by the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves - JORC Code, 2004 Edition. John Sainsbury has consented to the inclusion of this information in the form and context in which it appears.

**ABOUT CONSOLIDATED TIN MINES LIMITED**

Consolidated Tin Mines Limited (CSD) is a junior exploration company with current focus on Tin at Mt Garnet in the lower Herberton tin field in North Queensland.

Short to medium term goals are:

- Further expand resources at Gillian and Deadmans Gully while defining resources of known mineralisation at Pinnacles
- Develop a hard rock mining operation
- Develop an alluvial mining operation
- Explore other known mineralisation within current tenement holding to provide resource expansion

**Table 3: Gillian Tin intersections in excess of 10 metres**

<i>Hole No</i>	<i>Downhole Intercept</i>	<i>Length and Grade</i>
Hole 1	35-45 metres	10 metres @ 0.82% Sn, 38.3% Fe
Hole 4	14-27 metres	13 metres @ 2.02% Sn, 44.8% Fe
Hole 5	49-69 metres	20 metres @ 0.55% Sn, 25.3% Fe
Hole 7	14-35 metre	21 metres @ 1.14% Sn, 32.7% Fe
Hole 27	0-15 metres 45-58 metres	15 metres @ 1.31% Sn, 43.1% Fe 13 metres @ 0.59% Sn, 29.9% Fe
Hole 32	18-79 metres	61 metres @ 0.75% Sn, 31.0% Fe
Hole 77	60-70 metres	10 metres @ 0.6% Sn, 34.6% Fe
Hole 82	14-37 metres	23 metres @ 0.71% Sn, 41.8% Fe
Hole 83	16-43 metres	27 metres @ 1.1% Sn, 48.7% Fe
Hole 84	30-57 metres	27 metres @ 1.09% Sn, 43.7% Fe
Hole 93	20-30 metres	10 metres @ 0.88% Sn, 49.6% Fe
Hole 94	4-47 metres	43 metres @ 0.71% Sn, 34.3% Fe
Hole 95	34-70 metres	36 metres @ 1.2% Sn, 43.5% Fe
Hole 96	53-66 metres	13 metres @ 0.9% Sn, 31.7% Fe
Hole 104	8-18 metres	10 metres @ 0.81% Sn, 36.3% Fe
Hole 108	18-35 metres	17 metres @ 0.73% Sn, 38.9% Fe
Hole 109	17-28 metres	11 metres @ 0.74% Sn, 48.8% Fe
Hole 111	34-72 metres	38 metres @ 0.62% Sn, 31.8% Fe
Hole 113	6-37 metres	31 metres @ 0.62% Sn, 27.6 % Fe
Hole 127	72-95 metres	23 metres @ 1.01% Sn, 30.76% Fe
Hole 128	16-27 metres	11 metres @ 0.74% Sn, 26.9% Fe
Hole 129	9-33 metres	24 metres @ 1.45% Sn, 36.1% Fe
Hole 135	29-44 metres	15 metres @ 1.02% Sn, 39.6% Fe
Hole 136	48-68 metres	20 metres @ 0.84% Sn, 29.9% Fe

Stand out intersections are:-

<i>Hole No</i>	<i>Length and Tin Grade</i>
Hole 4	13 metres @ 2.02% Sn
Hole 7	21 metres @ 1.14% Sn
Hole 27	15 metres @ 1.31% Sn
Hole 32	61 metres @ 0.74% Sn
Hole 94	43 metres @ 0.71% Sn
Hole 111	38 metres @ 0.62% Sn
Hole 129	24 metres at 1.45% Sn (including 11 metres at 2.15% Sn - 1 Metre at 6.29% Sn)

**Table 4 – Breakdown of Iron and Fluorine JORC Resource**

<b>IRON (Fe)</b>	Measured tonnes	Grade %	Indicated tonnes	Grade %	Inferred tonnes	Grade %	Total tonnes	Grade %
Gillian	1,203,000	31.43	824,100	30.03	974,100	30.99	<b>3,001,200</b>	<b>30.90</b>
Pinnacles - Wafer	-	-	218,200	20.21	1,133,100	27.88	<b>1,351,300</b>	<b>16.87</b>
Pinnacles - Sniska	-	-	-	-	306,900	22.90	<b>306,900</b>	<b>22.90</b>
Pinnacles - Hartog	-	-	-	-	212,700	13.75	<b>212,700</b>	<b>13.75</b>
Deadmans Gully	-	-	401,500	34.89	-	-	<b>401,500</b>	<b>34.89</b>
<b>TOTAL</b>	<b>1,203,000</b>	<b>31.43</b>	<b>1,443,800</b>	<b>29.90</b>	<b>2,626,800</b>	<b>27.31</b>	<b>5,273,600</b>	<b>26.45</b>

<b>FLUORINE (F)</b>	Measured tonnes	Grade %	Indicated tonnes	Grade %	Inferred tonnes	Grade %	Total tonnes	Grade %
Pinnacles - Wafer	-	-	-	-	348,300	18.54	<b>348,300</b>	<b>18.54</b>
Pinnacles - Sniska	-	-	-	-	306,900	12.00	<b>306,900</b>	<b>12.00</b>
Pinnacles - Hartog	-	-	-	-	212,700	15.50	<b>212,700</b>	<b>15.50</b>
Pinnacles - Llahsram	-	-	-	-	91,700	13.00	<b>91,700</b>	<b>13.00</b>
<b>TOTAL</b>	<b>-</b>	<b>-</b>	<b>-</b>	<b>-</b>	<b>959,600</b>	<b>15.25</b>	<b>959,600</b>	<b>15.25</b>

Cut-off grade used was 5% Fe

#### **Resource Estimation Methodology**

The assay data from which this estimate is based was taken from a chip drilling reverse circulation (RC) program of 78 holes at the Gillian project, Drill samples were collected at one metre intervals and assay was completed on selected one metre samples. Assay method for tin, iron and fluorine was by XRF.

Resource blocks were polygonal shape outlines prepared on cross sections of drill assay information. Volume of Measured resource polygons were defined to 10 metres either side of the cross section centre line for the more confidently interpreted polygonal shapes. Volume of Indicated resource polygon were defined as strike continuous polygonal shapes continuous from measured resource blocks, for extents of between 10m-20m (or as 40-80 strike continuous drill defined polygonal outlines). Inferred resource outlines were defined by strike and dip continuity expectations based on the understandings from the better drilled areas.

Polygonal tin grade was an arithmetic average of drill assay results from within the polygon.

Density measurements for the tonnage conversions were measured from 17 core samples and 60 RC chip samples from the Gillian project, and the conservative average density was three (3) was used for the resource blocks.

**Table 5: Final assay results.**

Hole	Depth	Sn	Fe
H128			
	7-8	0.83 %	19.20 %
	8-9	1.25 %	30.70 %
	9-10	1.55 %	30.30 %
	10-11	1.74 %	38.90 %
	11-12	0.42 %	19.70 %
	12-13	0.27 %	20.10 %
	16-17	0.88 %	23.70 %
	17-18	1.09 %	32.50 %
	18-19	0.62 %	23.70 %
	19-20	0.88 %	26.60 %
	20-21	0.38 %	15.20 %
	21-22	0.85 %	27.20 %
	22-23	1.21 %	32.30 %
	23-24	0.73 %	22.50 %
	24-25	0.59 %	33.30 %
	25-26	0.58 %	42.60 %
	26-27	0.38 %	16.30 %

Hole	Depth	Sn	Fe
H129			
	9-10	0.27 %	16.40 %
	10-11	0.63 %	20.80 %
	11-12	0.95 %	24.00 %
	12-13	1.23 %	26.10 %
	13-14	1.29 %	23.40 %
	14-15	1.39 %	35.40 %
	15-16	6.29 %	35.20 %
	16-17	3.12 %	46.40 %
	17-18	2.30 %	48.80 %
	18-19	0.93 %	50.10 %
	19-20	2.25 %	38.60 %
	20-21	1.22 %	40.40 %
	21-22	1.24 %	46.60 %
	22-23	0.96 %	50.80 %
	23-24	1.24 %	40.10 %
	24-25	1.72 %	32.90 %
	25-26	2.42 %	41.60 %

	26-27	1.03 %	46.90 %
	27-28	0.46 %	31.80 %
	28-29	0.58 %	26.70 %
	29-30	0.88 %	35.80 %
	30-31	0.88 %	34.00 %
	31-32	0.82 %	38.50 %
	32-33	0.68 %	34.30 %

Hole	Depth	Sn	Fe
H130			
	83-84	0.93 %	29.40 %
	84-85	0.83 %	25.10 %
	85-86	1.53 %	57.60 %
	86-87	1.62 %	40.40 %
	87-88	1.29 %	27.10 %
	88-89	1.84 %	43.70 %
	89-90	0.57 %	16.30 %

Hole	Depth	Sn	Fe
H133			
	10-11	0.79 %	20.30 %
	11-12	0.74 %	17.90 %
	37-38	0.35 %	17.40 %
	38-39	0.67 %	18.50 %
	39-40	0.62 %	17.90 %
	40-41	1.89 %	19.70 %

Hole	Depth	Sn	Fe
H134			
	55-56	0.34 %	16.30 %
	56-57	0.44 %	16.40 %
	57-58	0.27 %	15.70 %
	58-59	0.23 %	13.70 %
	59-60	0.25 %	12.10 %
	108-109	0.28 %	9.90 %
	109-110	0.32 %	13.00 %
	110-111	0.30 %	13.70 %
	111-112	0.29 %	13.90 %
	112-113	0.35 %	14.20 %
	113-114	0.79 %	18.10 %

Hole	Depth	Sn	Fe
H135			
	11-12	0.44 %	21.50 %
	12-13	2.13 %	34.20 %
	13-14	0.69 %	35.90 %
	14-15	0.21 %	16.50 %
	29-30	0.44 %	27.80 %
	30-31	0.27 %	17.20 %
	31-32	0.33 %	27.20 %
	32-33	2.35 %	43.70 %
	33-34	1.47 %	39.00 %
	34-35	2.02 %	54.90 %
	35-36	1.08 %	40.10 %
	36-37	0.71 %	25.20 %
	37-38	0.36 %	18.60 %
	38-39	0.85 %	38.70 %
	39-40	1.36 %	49.00 %
	40-41	0.40 %	35.20 %
	41-42	0.53 %	37.70 %
	42-43	0.77 %	55.70 %
	43-44	0.76 %	41.10 %

66-67	0.75 %	33.10 %
67-68	0.69 %	23.10 %

Hole	Depth	Sn	Fe
H136			
	48-49	0.34 %	15.30 %
	49-50	0.67 %	22.40 %
	50-51	0.20 %	8.90 %
	51-52	0.07 %	8.90 %
	52-53	0.68 %	21.90 %
	53-54	1.20 %	29.00 %
	54-55	0.65 %	34.70 %
	55-56	0.63 %	50.00 %
	56-57	1.29 %	43.70 %
	57-58	1.38 %	35.90 %
	58-59	1.78 %	38.30 %
	59-60	0.86 %	32.30 %
	60-61	0.65 %	37.90 %
	61-62	1.03 %	26.10 %
	62-63	0.65 %	31.00 %
	63-64	0.99 %	44.10 %
	64-65	1.32 %	34.40 %
	65-66	0.99 %	27.50 %